

# Experimental study of convective heat transfer in a horizontal tube with insert using Nano fluids

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**Abstract**—Experimental investigation was carried out for tube side heat transfer coefficient, heat transfer enhancement, friction factor of CuO/water, Al<sub>2</sub>O<sub>3</sub>/water Nano fluids for turbulent flow in a copper circular tube fitted with perforated twisted tape insert. The copper tube of 15.6 mm outer diameter and 12.5 mm inner diameter and test length of 800 mm was used. Reynolds number varied in the range of 10000 – 35000. Size of squire hole in the twisted tape insert was 5.00 mm. Volume concentration of Nano fluid was varied from 0.05% to 0.3%. Heat transfer coefficient and Nusselt number from Gnielinski correlation [3] were compared with results of pure water, Nano fluids with and without insert. Heat transfer coefficient enhancement with respect to base fluid water at Reynolds number 3100, volume concentration of 0.3% found to be 37.2% without insert, 90.5% with insert and 127.2% with perforated insert in case of Al<sub>2</sub>O<sub>3</sub>/water Nano fluid and in case of CuO/water Nano fluid, 79.9% without insert, 113.5% with insert and 150.3% with perforated insert as compared to the base fluid, water.

**Keywords**— Heat exchanger, heat transfer enhancement, perforated twisted inserts, nanofluids

## Nomenclature

C<sub>p</sub> specific heat of fluid (J/kg K)  
d<sub>hyd</sub> hydraulic diameter of experimental tube (m)  
h heat transfer coefficient (W/m<sup>2</sup>K)  
k thermal conductivity (W/m K)  
m mass flow rate of the fluid (kg/s)  
Nu average Nusselt number = (h<sub>exp</sub>d<sub>hyd</sub>)/ k  
P tube periphery (m)  
Pr Prandtl number =  $\mu C_p/k$   
Q heat transfer rate (W)  
Re Reynolds number =  $\rho u d_{hyd}/\mu$   
S cross sectional area of the experimental tube  
T temperature (K)  
U fluid velocity (m/s)

## Greek letters

$\rho$  density (kg/m<sup>3</sup>)  
 $\mu$  Viscosity (kg/m s)  
 $\phi$  Volume fraction

## Subscripts

b bulk  
exp. Experimental  
in inlet  
nf nanofluid

out outlet  
p particle  
w wall

## I. INTRODUCTION

Design requirements for modern heat transfer equipment are high thermal performance and reduced size. In the past considerable research efforts were made to the development of advanced methods for heat transfer equipment. Conventional cooling fluids such as water, ethylene glycol, mineral oils widely used possess poor thermal conductivity. Considerable efforts have been made to improve the rate of heat transfer by using extended surfaces, micro channel etc. but further enhancement of cooling or heating is always in demand. A possible way of improving the heat transfer performance of conventional fluids is to suspend various types of small solid particles (size < 100 nm), metallic (eg. Cu, Ag, Al etc.) and non-metallic (e.g. Al<sub>2</sub>O<sub>3</sub>, CuO, Fe<sub>3</sub>O<sub>4</sub> etc.) particles in conventional fluids to form colloidal suspensions. Fluids suspended in them are called Nano fluids, and it was coined by Choi S. U. S. [1]. Nano fluid due to molecular chain behaviour, nanoparticles properly dispersed in the base fluid, achieved major benefits such as higher thermal conductivity, micro channel cooling without clogging, reduced chances of erosion and pumping power with enhancement in thermal conductivity and stability of mixture. In general, the above features in Nano fluids provide us new area of research in Nano fluid technology, plays an important role to improve heat transfer and energy efficiency in several areas including vehicular cooling in transportation, Power generation, defence, nuclear, microelectronics, biomedical devices. P. Promvong [2] experimentally investigated the convective heat transfer with conical rings inserts in a circular tube. The mean heat transfer rates obtained using diverging rings, converging-diverging rings and converging rings with diameter ratio  $d/D = 0.7 - 0.5$  (where d is small end diameter of conical ring and D is the diameter of test tube) were found to be 197- 333%, 138 – 234% and 91 – 175% more than those with plain tube respectively, Reynolds number range was 6000 < Re < 26000. For fixed Reynolds number, both Nu no. and friction increase with decrease in diameter. Khwanchit Wongcharee, Smith Eiamsa-ard [3] experimentally investigated heat transfer, friction and thermal performance characteristics of CuO/water Nano

fluid in a circular tube with twisted tape with alternate axis (TA). The concentration of Nano fluid was varied from 0.3 to 0.7 vol. %. The twist ratio of twisted tape was kept constant at 3. Experiment was carried out in laminar region Reynolds no. Range was 830 – 1990. With twisted tape Nusselt no. was improved up to 13.8 times of plain tube. Empirical correlations for heat transfer coefficient, friction factor and thermal performance are also developed. P. Bharadwaj A.D. et al. [4] experimentally determined heat transfer characteristics and pressure drop of flow of water in a spirally grooved tube with twisted tape insert. They considered laminar to fully turbulent range of Reynolds number. The grooves are clockwise with respect to the direction of flow. Heat transfer enhancement due to spiral grooves is further enhanced by twisted tape inserts. Bodius Salam, Suman Biswas [5] experimental investigation measuring heat transfer coefficient, friction factor, heat transfer enhancement of water for turbulent flow in a circular tube fitted with rectangular cut twisted tape insert was carried out under uniform heat flux. Reynolds number range was 10,000 – 19,000. Nusselt number obtained from smooth tube was compared with Gnielinski co-relation. With comparable Reynolds number, Nusselt no. was enhanced by 2.3 to 2.9 times at the cost of friction factor by 1.4 to 1.8 times compared to smooth tube. Alberto Garcia et al. [6] they carried out experimental study on three wire coils of different pitch inserts in a smooth tube in laminar and transition region. Friction factor lie between 5% to 40% in the fully laminar region. Reynolds number range 10- 2500, Pr. No range 200 – 700. Re no Below 200, wire coils do not enhance heat transfer with respect to smooth tube. For Re no Between 200 and 1000 with wire coils increase in heat transfer is observed. At Re no around 1000, wire inserts increase heat transfer coefficient up to 8 times with respect to smooth tube. A performance comparison between wire inserts and twisted tape inserts they stated that wire inserts perform better than twisted tapes in Re no range 700-2500. P. Sivashanmugam, S. Suresh [7] Experimental investigation of heat transfer and friction factor characteristics of laminar flow through a circular tube fitted with full length screw-tape of different twist ratios was carried out with uniform heat flux. They compared the heat transfer coefficient with increasing twist ratio with those obtained with plain tube data. Heat transfer coefficient increases with the twist ratio. Friction factor also increases with twist ratio. K. B. Anoop et. al. [8] carried out experimental investigation on convective heat transfer characteristics in the developing region of tube flow with constant heat flux with  $Al_2O_3$ /water Nano fluid. Main objective was to study the effect of particle size on convective heat transfer. They selected two nanoparticles of average

size 45 nm and 150 nm. They observed that Nano fluid with Nano fluid with 45 nm particle size showed higher heat transfer coefficient than that with 150 nm size.

They also observed that in the developing region, heat transfer coefficient enhancement is higher than in the developing region. Nano fluid concentration results increase in effective thermal conductivity. Besides, heat transfer enhancement is associated with particle motion in the form of Brownian motion[9] by which the particle move through the liquid and possible collide, enabling solid to solid transportation of heat from particle to particle, and expecting increase in thermal conductivity. Other concept is of Nano-convection of fluid around particles due to their motion, particle transport some of the amount of heat transferred through agitation in the liquid. Mangrulkar C. K. et al. [10] experimentally investigated heat transfer enhancement in the laminar and transition fluid flow through copper tube with constant heat flux.  $Al_2O_3$ /water and  $CuO$ /water Nano fluids with volume concentration range 0.1% to 0.5%. In each case they found that optimum enhancement in heat transfer is observed at relatively lower volume concentration ranging between 0.2 to 0.3%.

## OBJECTIVE OF THE WORK

The main objective of work was experimental investigation of heat transfer enhancement in horizontal tube using Nano fluids. The nanoparticles,  $Al_2O_3$  and  $CuO$ , were selected, as metallic oxides are cheaper than metallic one, though metals have much higher thermal conductivity than metallic oxides and therefore, higher heat transfer enhancement. Base fluid chosen was distilled water.

## II. EXPERIMENTAL SET UP

Fig.1 shows the schematic of experimental set up used in the present research to investigate the convective heat transfer of Nano fluids in a horizontal circular tube heated with uniform heat flux. Flow lines include reservoir tank, heater, pump, flow meter, duct, thermocouples, and cooling unit. The pump gives constant flow rate. The flow rate in the test section is regulated by adjusting the bypass valve located in the recycle line. Test section is a smooth horizontal copper tube, ID 12.5 mm, OD 15.8 mm and length 800 mm, electrically insulated nikrome heating wire was uniformly wound along the length of the tube. The terminals of nikrome wire were connected to the variac transformer. Thermocouples were tapped along the tube wall for monitoring the local temperatures of the surface tube wall. Thermometers will measure the inlet and outlet temperatures of working fluid. The heating tube and thermocouples were covered with insulation to minimize heat loss to the surrounding. The rota meter will measure the required flow rates of the fluid. Cooling unit at the exit section will cool the test fluid to the inlet temperature. To measure the pressure drop along the test section a manometer was used.

Experiment was conducted first with distilled water, the base fluid of a  $\text{Al}_2\text{O}_3$  and  $\text{CuO}$  nanoparticles, with varying mass flow rates 4, 6, 8, 10, and 12 litters/min., then with  $\text{CuO}$ /water Nano fluid and same mass flow rates as with water and volume concentrations 0.05%, 0.08%, 0.1% and 0.3%. Next, the experiment was repeated with twisted tape insert with no perforations and same volume concentrations. The twisted tape was four in numbers. The experiment was repeated with squire perforated tape insert and same volume concentrations.

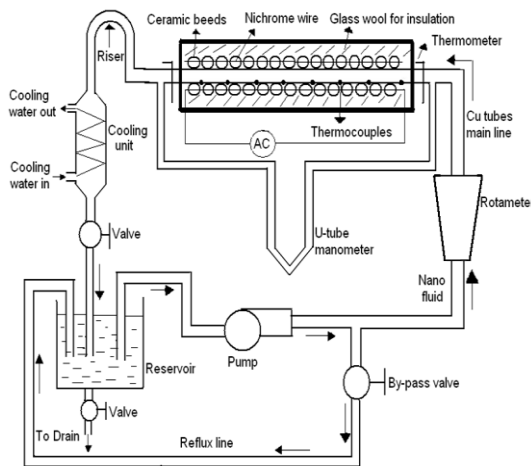


Fig.1 Experimental set up [11]

### III. NANOFLUID PREPARATION

The first step in experimental studies is the preparation of Nano fluids. Preparation of a stabilized Nano fluid is of great importance in heat transfer applications of Nano fluids. Poorly prepared Nano fluids will render biphasic heat transfer (i.e. solid-liquid). Dispersant or surfactant was not added as they may change the properties of the Nano fluid. Nano fluids were prepared with nanoparticles  $\text{Al}_2\text{O}_3$  and  $\text{CuO}$  (average size 45 nm) with deionized water as base fluid. The nanoparticles were purchased from Sigma Aldrich, Germany. Specific quantities of nanoparticles were mixed with distilled water as the base fluid for both and stirred with magnetic stirrer for about eight hours. The stirred Nano fluid was kept for about 24 hrs. and no sedimentation was observed. Immediately the experiment was started. The Nano fluids with four different  $\text{Al}_2\text{O}_3$  and  $\text{CuO}$  nanoparticle concentration (0.05%, 0.08%, 0.1% and 0.3% volume fraction) were prepared to study the convective heat transfer in a tube.

### IV. NANOFLUID PROPERTIES

Thermo physical properties of the Nano fluid must be known before using for experimental test. The nanoparticles are assumed to be well dispersed in the base fluid and concentration of nanoparticles is assumed to be uniform throughout the tube. This assumption is not true in real systems because the particles migrate in the tube. However, the assumption is useful tool to evaluate the physical properties of a

Nano fluid. The thermo-physical properties of prepared Nano fluids are calculated from water and nanoparticles characteristics at mean inlet and outlet bulk temperatures. The following correlations for thermal conductivity, density, specific heat, viscosity [2] are used.

The density of Nano fluids can be predicted by mixing theory as:

$$\rho_{nf} = (1 - \phi) \rho_{bf} + \phi \rho_{np} \quad (1)$$

$$k_{nf}/k_{bf} = [k_{np} + 2k_{bf} + 2(k_{np} - k_{bf})(1 + \beta)^3\phi] / [k_{np} + 2k_{bf} - (k_{np} - k_{bf})(1 + \beta)^3\phi] \quad (2)$$

Some researchers have used the following equation which is same approach as to the mixing theory for an ideal

$$(Cp_{nf} \cdot \rho_{nf}) = \phi (Cp_{np} \cdot \rho_{np}) + (1 - \phi) (Cp_{bf} \cdot \rho_{bf}) \quad (3)$$

$$\mu_{nf} = \mu_{bf}(1 + 2.5\phi) \quad (4)$$

In the above equations, the subscripts "nf", "np" and "bf" refer to the Nano fluid, nanoparticle and base fluid respectively.  $\phi$  is the volume fraction of the nanoparticles added to base fluid.  $\beta$  is the Nano layer thickness to the original particle radius. This can be taken as 0.1 to calculate the Nano fluid effective thermal conductivity.

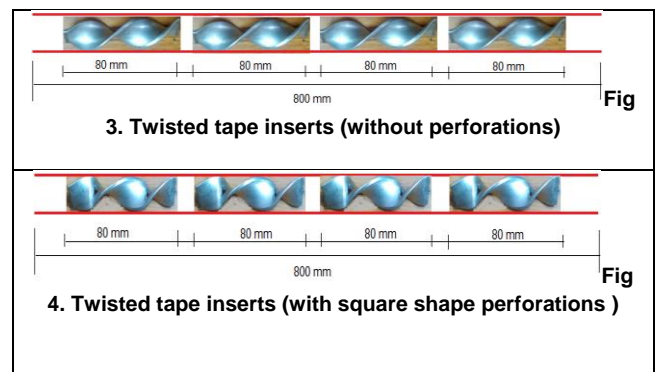


Fig. 2 Arrangement of Inserts inside Copper Tube

### V. DATA ANALYSIS

Observations were taken at steady state conditions. Initially experiment was performed with distilled water at various mass flow rates and then for  $\text{Al}_2\text{O}_3$ /water and  $\text{CuO}$ /water Nano fluids with volume concentrations 0.1-0.7%. Flow rates were same for all three fluids. Constant heat flux was maintained in all the cases. According to the Newton's law of cooling,

$$Q = h_{exp} A (T_w - T_b) \quad (5)$$

Where mean bulk temperature is given by

$$T_b = (T_{in} + T_{out})/2$$

Where  $T_{in}$  = inlet temperature of fluid

$T_{out}$  = outlet temperature of fluid

Heat transfer rate,  
 $Q = m C_{pnf} (T_{out} - T_{in})$  (6)

Equating (5) & (6)

$$h_{exp} A (T_w - T_b) = m C_{pnf} (T_{out} - T_{in})$$

$$h_{exp} = [m C_{pnf} (T_{out} - T_{in})] / [A (T_w - T_b)]$$
 (7)

$$Nu = (h_{exp} D_{hyd}) / k$$

$$D_{hyd} = 4S/P$$

All the physical properties are evaluated at bulk mean temperature  $T_b$ , of the fluid.

## VI. RESULT AND DISCUSSION

Experimental results are compared with Dittus-Boelter (eq.8) and Gnielinsky (eq. 9) correlations,

$$Nu = 0.023 Re^{0.8} Pr^{0.4}$$
 (8)

$$Nu = [(f/8) (Re - 1000) Pr] / [1 + 12.7 (f/8)^{0.5} (Pr^{2/3} - 1)]$$
 (6)

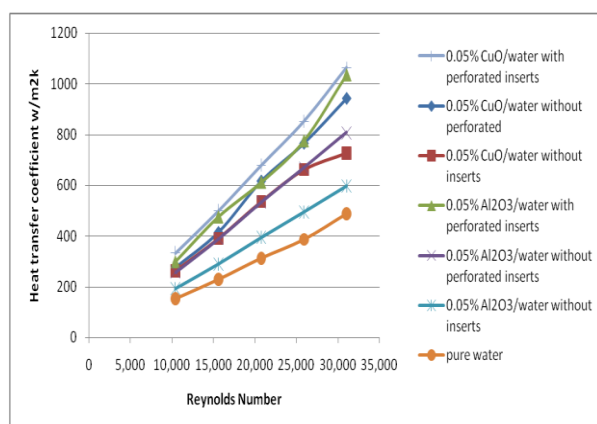
$$3000 \leq Re \leq 5 \times 10^6 \text{ and } 0.5 \leq Pr \leq 2000$$

Where, from Petukhov, 1970, friction factor  $f$ , was calculated using equation (6)

$$f = (0.79 \ln Re - 1.69)^{-2}$$
 (6)

From fig. 3 (volume concentration 0.05%), it is observed heat transfer coefficient increases with increase in Reynolds number. Heat transfer coefficients are higher than pure water in case of both of the Nano fluids. They are higher for twisted tape inserts. This is because twisted tape inserts create turbulence in the flowing fluid causing enhancement of heat transfer. Perforated twisted tape inserts enhance heat transfer coefficients further than without perforations. Perforations cause increase in turbulence further causing increase in heat transfer, but at the cost of pressure drop. Further, heat transfer coefficients are higher in case of CuO/water Nano fluid than  $Al_2O_3$ /water. Similar trend is observed for higher volume concentrations (figs. 4, 5 and 6).

For 0.3vol % (fig.6) and Reynolds number 31000, with  $Al_2O_3$ /water Nano fluid, the heat transfer coefficient enhancement w.r.t. water is 37.2%, 90.5% with twisted tape inserts, 127.2% with perforated twisted tape inserts. In case of CuO/water Nano fluid, the enhancements are 79.9%, 113.5% and 150.3% respectively.



At Reynolds number 1000 (fig.6), with  $Al_2O_3$ /water Nano fluid, the heat transfer coefficient enhancement w.r.t. water is 42.4%, 82.1% with twisted tape inserts and 117.2% with perforated twisted tape inserts. In case of CuO/water Nano fluid, the enhancements are 127.1%, 135.1% and 163.5% respectively.

Fig. 3 Heat transfer coefficient Vs Reynolds Number for pure water and 0.05% loading of  $Al_2O_3$  and CuO with pure water. (All cases)

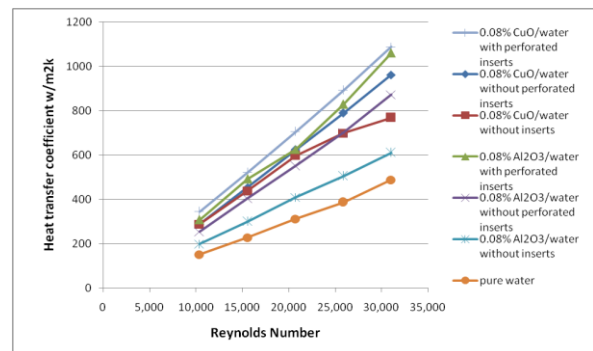


Fig. 4 Heat transfer coefficient Vs Reynolds Number for pure water and 0.08% loading of  $Al_2O_3$  and CuO with pure water. (All cases)

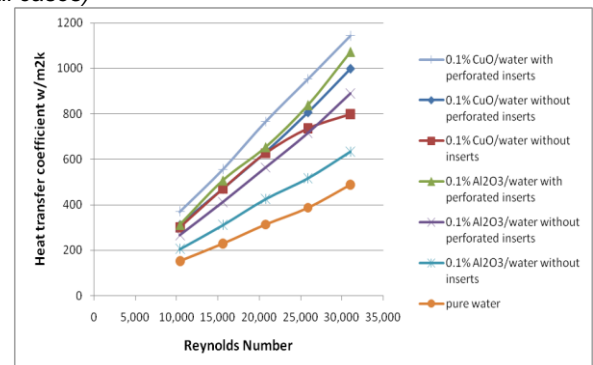


Fig. 5 Heat transfer coefficient Vs Reynolds Number for pure water and 0.1% loading of  $Al_2O_3$  and CuO with water. (All cases)

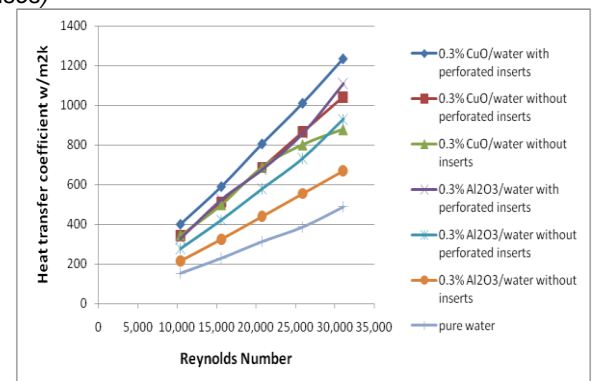


Fig. 6 Heat transfer coefficient Vs Reynolds Number for pure water and 0.3% loading of  $Al_2O_3$  and CuO with water. (All cases)

Figures (7, 8, 9 and 10) show the graphs friction factor Vs Reynolds number for  $Al_2O_3$ /water and CuO /water Nano fluids for volume concentrations of 0.05% - 0.3%. Friction factor decreases with increase in Reynolds number. Trend is same in all cases.



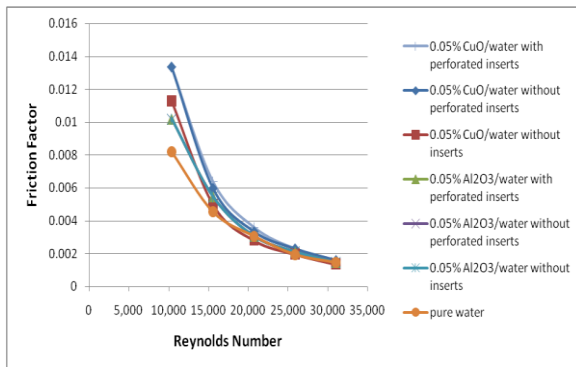


Fig. 7 Friction Factor Vs Reynolds Number for pure water and 0.05 % loading of  $\text{Al}_2\text{O}_3$  and CuO with water. (All cases)

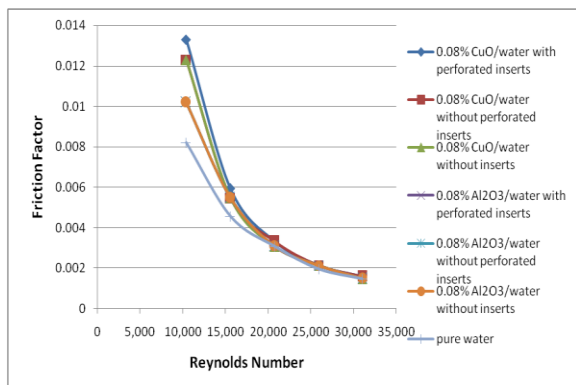


Fig. 8 Friction Factor Vs Reynolds Number for pure water and 0.08 % loading of  $\text{Al}_2\text{O}_3$  and CuO with water. (All cases)

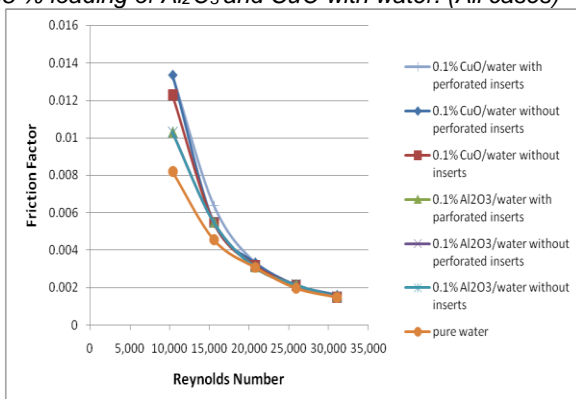


Fig. 9 Friction Factor Vs Reynolds Number for pure water and 0.1 % loading of  $\text{Al}_2\text{O}_3$  and CuO with water. (All cases)

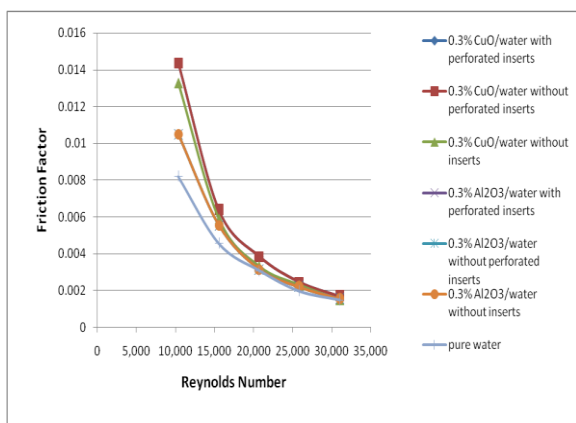


Fig. 10 Friction Factor Vs Reynolds Number for pure water and 0.3 % loading of  $\text{Al}_2\text{O}_3$  and CuO with water. (All cases)

For lower Re no., for CuO/water Nano fluid friction factor is higher than  $\text{Al}_2\text{O}_3$ /water Nano fluid. At higher Re no. friction factor is almost same for both the Nano fluids. This trend is same for all volume concentrations. At lower Re no. friction factor is higher for Nano fluid than for pure water. However at higher Re no. difference is not significant.

Fig.(11,12,13 and 14) show the graphs, Nu no. Vs Re no with increasing volume concentration. Nu no. increase with Re no. This trend is same for all volume concentrations. At comparable Re no Nu nos. is higher for higher volume concentration

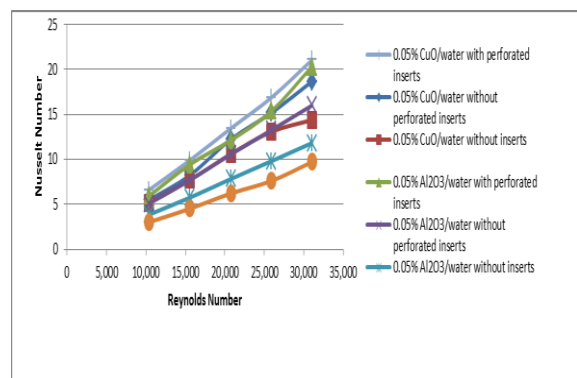


Fig. 11 Nusselt Number Vs Reynolds Number for pure water and 0.05% loading of  $\text{Al}_2\text{O}_3$  and CuO with water. (All cases)

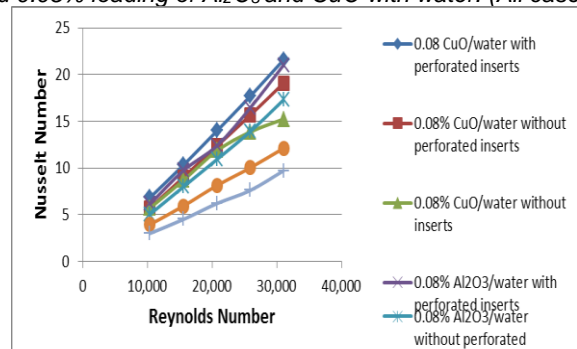


Fig. 12 Nusselt Number Vs Reynolds Number for pure water and 0.08% loading of  $\text{Al}_2\text{O}_3$  and CuO with water. (All cases)

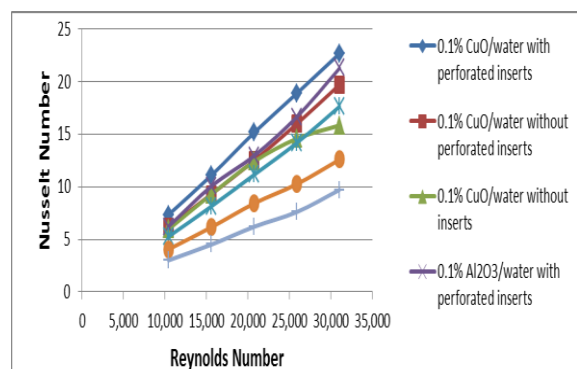


Fig. 13 Nusselt Number Vs Reynolds Number for pure water and 0.1% loading of  $\text{Al}_2\text{O}_3$  and  $\text{CuO}$  with water. (All cases)

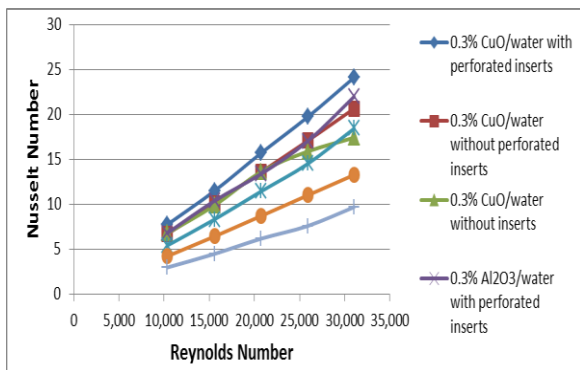


Fig. 14 Nusselt Number Vs Reynolds Number for pure water and 0.3% loading of  $\text{Al}_2\text{O}_3$  and  $\text{CuO}$  with water. (All cases)

For the validation of experimentation, theoretical heat transfer coefficient is compare with the experimental values. In this experimentation, the value of Reynolds number is ranging from 10000 to 35000 hence, From Gnielinski, 1976 equation [3] is used to find theoretical Nusselt number. From fig.18 it is observed that, theoretical Nusselt number is greater as compare to the experimental values for 0.3 vol. %  $\text{Al}_2\text{O}_3$ /water Nano fluids and 0.3 vol. % of  $\text{CuO}$ /water Nano fluids. In the experimentation, with and without perforated twisted tape inserts is use which causes the more Nusselt number difference between theoretical and practical values. Nusselt number of perforated twisted tape inserts is more as compare to other conditions. It is just because of provision of inserts wit perforations in the flow stream which increase turbulence results increase Nusselt number. It is observed that, Nusselt number increases rapidly when mass flow rate increases. From fig.15 it is observed that, theoretical  $h$  is greater as compare to the experimental values for 0.3 vol. %  $\text{Al}_2\text{O}_3$ /water Nano fluids and 0.3 vol % of  $\text{CuO}$ /water Nano fluids. In the experimentation, with and without perforated twisted tape inserts is use which causes the more heat transfer coefficient difference between theoretical and practical values. Heat transfer coefficient of perforated twisted tape inserts is more as compare to other conditions. It is just because of provision of inserts with perforations in the flow stream which increase turbulence results increase in heat transfer coefficient if rapidly increasing in mass flow rate.

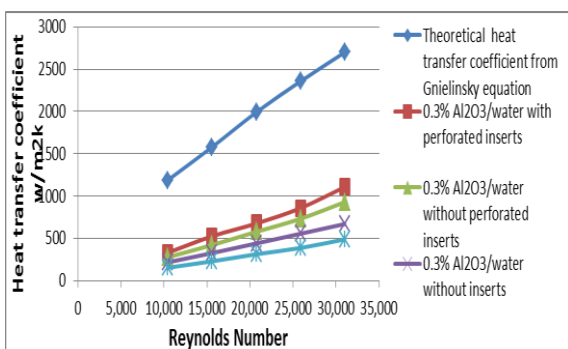


Fig.15 Heat transfer coefficient Vs Reynolds Number for 0.3%  $\text{Al}_2\text{O}_3$ /water Nano fluid

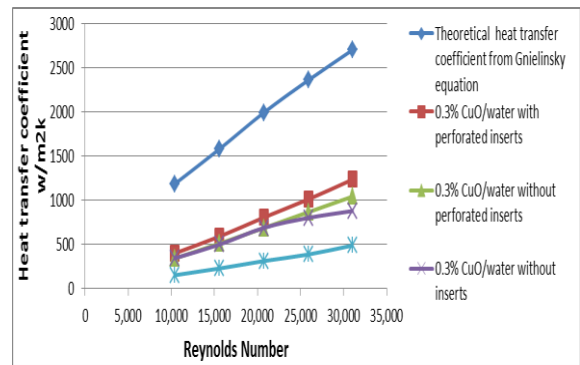


Fig.16 Heat transfer coefficient Vs Reynolds Number for 0.3%  $\text{CuO}$ /water Nano fluid

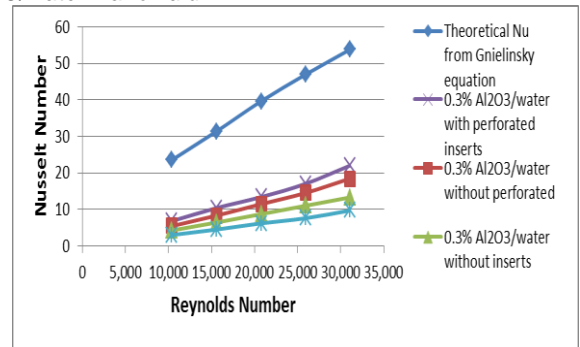


Fig.17 Nusselt Number Vs Reynolds Number for 0.3%  $\text{Al}_2\text{O}_3$ /water Nano fluid

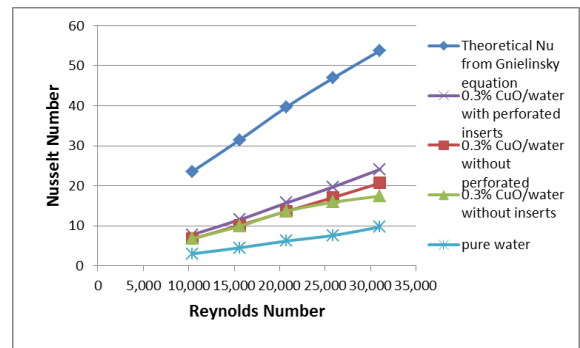
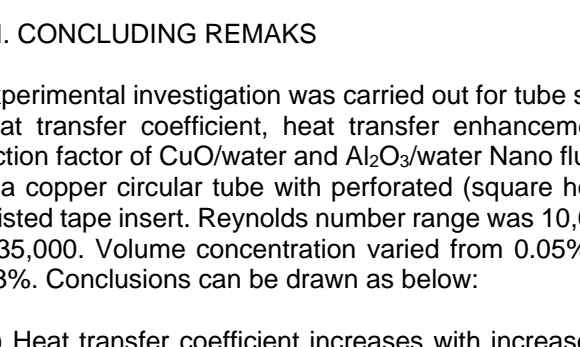


Fig.18 Nusselt Number Vs Reynolds Number for 0.3%  $\text{CuO}$ /water Nano fluid



(1) Heat transfer coefficient increases with increase in Reynolds number.

(2) Heat transfer coefficients with both Nano fluids improved than with pure water.

## VII. CONCLUDING REMAKS

Experimental investigation was carried out for tube side heat transfer coefficient, heat transfer enhancement, friction factor of  $\text{CuO}$ /water and  $\text{Al}_2\text{O}_3$ /water Nano fluids in a copper circular tube with perforated (square hole) twisted tape insert. Reynolds number range was 10,000 – 35,000. Volume concentration varied from 0.05% to 0.3%. Conclusions can be drawn as below:

(3) Heat transfer coefficients are higher for twisted tape inserts for both Nano fluids compared to Nano fluid alone. This is because twisted tape inserts create turbulence in the flowing fluid.

(4) Perforated twisted tape inserts further enhance heat transfer coefficients but at the cost of pressure drop.

(5) Heat transfer coefficients are higher for CuO/water Nano fluid than Al<sub>2</sub>O<sub>3</sub>/water Nano fluid.

(6) At lower Re nos. the friction factors are higher for CuO/water Nano fluid than Al<sub>2</sub>O<sub>3</sub>/water Nano fluid. However, at higher Re no. there is no noticeable difference.

(7) At lower Re no. the friction factor is higher for Nano fluids than pure water. However this difference is insignificant at higher Re nos. Nano fluid with enhanced thermal conductivity brings about enhanced heat transfer. In additions, other suitable conditions as nanoparticle material, appropriate particle concentrate in range, particle size affect the enhancement of the heat transfer coefficient. Suspended nanoparticles increase the surface area and thermal conductivity of suspensions increase with the ratio of surface area to volume of the nanoparticle and hence increase in heat transfer rate.

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